A study of particulate matter concentration released during laser paint removal process on car coated substrate

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Abstract: Normalization mass (N) of particulate matter (PM) per one laser shot and 1.0 cm² beam size released during the laser irradiation were measured on three different types of car coated substrate samples A, B and C by using DustTrak Aerosol Monitor 8520. The highest N of $PM_{1.0}$ and $PM_{10.0}$ were 0.0485 mg/shot/cm² and 0.0766 mg/shot/cm² for Sample A, 0.0890 mg/shot/cm² and 0.1728 mg/shot/cm² for Sample B and 0.0530 mg/shot/cm² and 0.0634 mg/shot/cm² for Sample C, respectively. Laser paint removal technique is considered safe than conventional chemical stripping process in term of health implications prevention and safety managements.

Keywords: Particulate matter, DustTrak 8520, Nd:YAG laser, Paint removal, Car coated substrate

I. Introduction

Chemical paint stripping process was intractable in preventing the health implications to the staff incharged due to continuous production of hazardous chemicals component as by-products sort of methylene chloride, phenolic compounds, activated acids, bases free from phenols and chromates and many more [1]. Conversely, health effects and environment pollution in laser paint removal is considered minimal in term of producing toxic, air contaminants, particulate matter, various metal particles and hazardous waste compare to conventional chemical techniques. However, the severe implications to these conditions is still exist [2, 3]. This is due to tiny population of spherical and aggregates particulate matter (PM) ranged from nano to submicron particles was released from interaction between laser beam and target of painted layer during laser paint removal [4-6]. The emission rate of this hazardous substances is highly depending on the thickness and physical condition of the unwanted surface layer [7]. Clean Air Act (CAA) of USA declared PM is one of six major air pollutants and becomes the main factor for the establishment of National Ambient Air Quality Standards (NAAQS) by EPA [8].

PM could be either existed as solid particles or liquid droplets in a wide range of sizes [9, 10]. Aerosol PM with diameter less or equal to a nominal 10 μ m but greater than 2.5 μ m is known as PM_{10.0}. PM_{10.0} accumulates in the upper respiratory tract to the lower respiratory system and can caused illness. In addition, aerosol PM with diameter less or equal to a nominal 1.0 μ m is known as PM_{1.0} [9, 11].

Directly exposure to these aerosols of PM not only influenced the laser stripping process efficiency but more worst is increased the health risk of operators incharged [4, 5]. Primary route of PM exposure is through inhalation and secondarily is through ingestion [9]. Acute and chronic exposure to aerosol PM leads to detrimental health effects [9, 10]. Main portal entry for PM is lung, thus the interaction of PM with respiratory epithelium and alveolar macrophages will then induced the health risk to the pulmonary disease [8]. This condition becomes the main factors to aggravate lung disease sort of asthma and chronic obstructive pulmonary disease (COPD) which leads to cause lung cancer and cardiac problems [9, 12]. Ultrafine PM is identified as highly toxic and poses the largest health risk due to its ability to migrate and deposit deep into the lung and risked the whole of respiratory system [8, 13].

The recommended values for annual and 24-hour mean concentrations are $20 \times 10^{-3} \text{ mg/m}^3$ and $50 \times 10^{-3} \text{ mg/m}^3$ for PM₁₀₀ and 10 x 10^{-3} mg/m^3 and 25 x 10^{-3} mg/m^3 for PM_{2.5} [14, 15]. There was no specific guideline for PM_{1.0} carried out from WHO, but the recommended mean concentration value for this particulate type should be less than 25 x 10^{-3} mg/m^3 for short term exposure. Nevertheless, the scientific recommendation for interim target values of PM from WHO was done in open air which based on the selected certain cities in the world, not in the workplace. In addition, the health risk due to hazardous PM is considered to highly dependent on the air exchange in the workplace, the size of the workplace, the way of spreading, distribution, compositions and types of the PM itself. There should have the threshold limit value (TLV) in the workplace as suggested by Kusch et al. (2003), which was 6 mg/m³ for totally independent of the chemical compositions of respirable dust [7]. But, there were no previous studies carried out regarding to the relationship between the size of workplace with the concentrations and distributions of PM released.

To address this issue, a study to determine normalization mass (N) of PM per one laser shot and 1.0 cm² beam size released during the laser irradiation were done on three types of car coated substrate samples in a closed space. The experiment was carried out at Medical Physics Laboratory, School of Physics, Universiti Sains Malaysia, Penang.

II. Experimental Set-Up

Prior start the experiment, paint thickness for substrate samples of car models A, B and C were determined by using CEM DT-156 Paint Coating Thickness Gauge Tester F/NF Probe which ranged from $92 - 134 \mu m$, $196 - 450 \mu m$, $219 - 283 \mu m$, respectively and never repaints. A total 54 car coated substrate with consist of 18 samples by each type were irradiated by using Cynosure Cynergy Pulse Nd:YAG laser. Ten spotted laser irradiation was done on each substrate sample with 10 J/cm² increments of laser fluence (*F*) by manipulating the pulse width (PW), repetition rate (RR) and beam size (BS) as listed in the Table 1 and Fig. 1.

Table 1: Laser parameters considered for 3 mm and 5 mm BS with varies in F, PW and RR.

					- ,
Sample	Number of	BS	F	PW	RR
number	irradiation	(mm)	(J/cm^2)	(ms)	(Hz)
1	10	3	210 - 300	100	1.0
2	10	3	210 - 300	200	1.0
3	10	3	210 - 300	300	1.0
4	10	3	210 - 300	100	1.5
5	10	3	210 - 300	200	1.5
6	10	3	210 - 300	300	1.5
7	10	3	210 - 300	100	2.0
8	10	3	210 - 300	200	2.0
9	10	3	210 - 300	300	2.0
10	10	5	150 - 240	100	1.0
11	10	5	150 - 240	200	1.0
12	10	5	150 - 240	300	1.0
13	10	5	150 - 240	100	1.5
14	10	5	150 - 240	200	1.5
15	10	5	150 - 240	300	1.5
16	10	5	60 - 150	100	2.0
17	10	5	60 - 150	200	2.0
18	10	5	60 - 150	300	2.0

Note: Maximum *F* for 3 mm BS is 300 J/cm² for all laser parameters. Meanwhile the maximum *F* for 5 mm BS is 240 J/cm² set-up with RR 1.0 and 1.5 Hz whereas 150 J/cm² set-up with RR 2.0 Hz.



Figure 1: Experimental set-up for laser paint removal on the car coated substrate.

 $PM_{1.0}$ and $PM_{10.0}$ were measured during laser paint removal process by using DustTrak Aerosol Monitor 8520. Both PM measurements were based on 10 minutes counting started from first irradiation on each certain substrate samples. For this study, some selection parameters were programmed to the DustTrak 8520 by using TrakPro software which were; (a) Time constant, (b) Logging interval and (c) Date and real-time clock.

Time constant is the average counting of PM within a certain period set-up. For this research, time constant was fixed at 1.0 s for all measurement means the PM detected actually was the average countings updated every second within a certain period. Meanwhile, logging interval was the time duration set-up to obtain a total of average PM countings. For all PM measurement, logging interval was set-up for 10 minutes; means a total of average countings (time constant) was obtained after 10 minutes measurements (logging

interval). Date and real-time clock were synchronized to the current date and clock of the connected computer and updated automatically for countings identification. To ensure the validation data obtained, the device was calibrated to the standard requirement once equipped with the inlet nozzle by considering two calibration factors which were; (a) Re-zeroing, (b) Flow rate.

Re-zeroing process was done once changed the inlet nozzle in order to reset the internal circuit from kept track a total of aerosol quantity that had gone through the instrument. To re-zeroing the device, the zero filter was equipped to the sample inlet as shown in Fig. 2. By setting the DustTrak in survey mode, pressed and hold the calibrated button until the display counts to zero. Released the button immediately when the counts zero was reached and "calibrate zero" will be appeared on the display screeen. Pressed the sample button and wait for 60 s countdown to determine the current calibration value. If the displayed value was between - 0.001 to $+ 0.001 \text{ mg/m}^3$, the device does not need any adjustment.



Figure 2: Re-zeroing of the DustTrak 8520 for new inlet nozzle installation.

Flow rate through the DustTrak monitor was set-up by connecting the flow meter tube to the sample inlet as shown in Fig. 3. By keeping the device in survey mode, the flow meter was adjusted by turning the flow adjustment screw located on the front top of the instrument. The factory setting for this calibration was 1.7 L/min.



Figure 3: Flow rate of the DustTrak was set-up by using flow meter at 1.7 L/min.

Two DustTrak 8520 aerosol monitor was used together with the required inlet nozzle for specific size measurement of $PM_{1.0}$ and $PM_{10.0}$, respectively. $PM_{1.0}$ and $PM_{10.0}$ were measured in a close wood box with size 60.5 cm length, 40.5 cm wide and 40.5 cm height. The experimental set-up for this study was shown in Fig. 4.

A study of particulate matter concentration released during laser paint removal process on car coated



Figure 4: Experimental set-up of DustTrak 8520: a. DustTrak 8520 was set-up for PM_{10.0} and ready for measurement b. DustTrak 8520 was set-up for PM_{1.0} and ready for measurement.

III. Results And Discussions

Concentration of PM or aerosol by-products from laser paint removal process is depending on physical and chemical compositions of the ablated paint material and the laser parameters were used sort of F, PW, RR and BS [5, 7, 16]. The aerosols generated during the laser paint removal process were characterized in term of size distributions (PM_{1.0} and PM_{10.0}) and average of particle mass concentrations.

By assuming the spatial distributions of energy is homogenous for each shot on the painted material, it is possible to normalize the measurements with respect to the interaction of surface area [17]. Thus, each measurement of particle mass is related to one laser shot and 1.0 cm² of ablated paint. (1) depicts the averaging method which was used to acquired the mass of particles, N [5].

$$N = d_f \mathbf{x} \left(\mathbf{C}_{Av} - \mathbf{C}_{\text{noise}} \right) \mathbf{x} \ Q \mathbf{x} \ \Delta_t / \left(n_{\text{shots}} \mathbf{x} \ A \right)$$
Eq. 1

Where *N* is normalization mass of PM per one laser shot and 1.0 cm² (mg/shot/cm²), d_f is the dilution factor, C_{Av} (mg/m³) is the average concentration issued from the measurement device during Δ_t , C_{noise} (mg/m³) is the average concentration issued before laser shoots, Q (m³/min) is the constant air flow rate of the device, Δ_t (min) is the time interval for the PM accounted, n_{shots} is the number of laser shoots within Δ_t and A (cm²) is the irradiated crater area. For this analysis, the dilution factor d_f is assumed to fix at value 1 due to no diluter was build in to the DustTrak 8520.

PM concentration measurements results were classified into 3 main parts based on the 3 types of samples A, B and C as shown in Fig. 5, 6 and 7, respectively. Each part has 2 types of PM results, which were $PM_{1.0}$ and $PM_{10.0}$. The average of PM determined from the graph was applied in the (1) to obtain the *N* for each substrate sample A, B and C as shown in Table 2.



Figure 5: Normalization mass (*N*) of PM_{1.0} and PM_{10.0} for substrate sample A1 - A18. The highest *N* of PM_{1.0} and PM_{10.0} were 0.0485 mg/shot/cm² and 0.0766 mg/shot/cm² obtained from substrate sample A9.



Figure 6: Normalization mass (*N*) of PM_{1.0} and PM_{10.0} for substrate sample B1 - B18. The highest *N* of PM_{1.0} and PM_{10.0} were 0.0890 mg/shot/cm² and 0.1728 mg/shot/cm² obtained from substrate sample B6.



Figure 7: Normalization mass (*N*) of PM_{1.0} and PM_{10.0} for substrate sample C1 - C18. The highest *N* of PM_{1.0} and PM_{10.0} were 0.0530 mg/shot/cm² and 0.0634 mg/shot/cm² obtained from substrate sample C17 and C8.

Sample	RR	Н	d.	$O(m^{3}/min)$	<i>n</i> .	Δ_{t}	Α	C_{noise}	Types	$C_{\rm av}$	$N(mg/shot/cm^2)$
Sample	(Hz)	(%)	u_f	Q (III / IIIII)	<i>n</i> _{shots}	(min)	(cm^2)	(mg/m^3)	of PM	(mg/m^3)	N (Ing/shot/chi)
A1	1	73	1	0.0017	10	10	0.071	0.003	$PM_{1.0}$	<mark>0.693</mark>	0.0166
	1	15		0.0017	10	10	0.071	0.005	$PM_{10.0}$	1.598	0.0384
A2	1	71	1	0.0017	10	10	0.071	0.005	$PM_{1.0}$	0.948	0.0227
		71	•	010017	10	10	01071	01002	$PM_{10.0}$	2.052	0.0493
A3	1	71	1	0.0017	10	10	0.071	0.006	$PM_{1.0}$	1.81	0.0434
	-								$PM_{10.0}$	2.575	0.0619
A4	1.5	73	1	0.0017	10	10	0.071	0.004	$PM_{1.0}$	1.031	0.0247
									$PM_{10.0}$	2.291	0.0551
A5	1.5	71	1	0.0017	10	10	0.071	0.005	$PM_{1.0}$	1.067	0.0256
						- 0			$PM_{10.0}$	2.131	0.0512
A6	1.5	77	1	0.0017	10	10	0.071	0.001	$PM_{1.0}$	1./1/	0.0413
									$PM_{10.0}$	2.856	0.0687
A7	2	74	1	0.0017	10	10	0.071	0.002	PM _{1.0}	1.388	0.0334
									PM _{10.0}	2.798	0.0075
A8	2	73	1	0.0017	10	10	0.071	0.003	PM1.0 DM	1.240	0.0299
									PIVI _{10.0}	2.162	0.0323
A9	2	74	1	0.0017	10	10	0.071	0.002	PIVI1.0 DM	2.018	0.0465
									P IVI _{10.0}	3.165	0.0700
A10	1	73	1	0.0017	10	10	0.196	0.004	DM	2 505	0.0133
									DM	2.505	0.0217
A11	1	72	1	0.0017	10	10	0.196	0.004	PM	2 453	0.0155
									PM	1.462	0.0212
A12	1	71	1	0.0017	10	10	0.196	0.002	PM ₁₀₀	2 794	0.0120
									PM ₁₀	2.098	0.0242
A13	1.5	72	1	0.0017	10	10	0.196	0.005	PM100	3 884	0.0336
									PM ₁₀	1.298	0.0112
A14	1.5	72	1	0.0017	10	10	0.196	0.004	PM100	2.545	0.0220
		-		0.0015	10	10	0.105	0.000	PM_{10}	1.731	0.0150
A15	1.5	76	1	0.0017	10	10	0.196	0.003	PM10.0	3.386	0.0293
									PM_{10}	3.167	0.0274
A16	2	74	1	0.0017	10	10	0.196	0.003	PM10.0	3.516	0.0304
. 17	2	70		0.0017	10	10	0.106	0.005	$PM_{1,0}$	2.65	0.0229
A17	2	12	1	0.0017	10	10	0.196	0.005	$PM_{10.0}$	3.145	0.0272
A18	2	74	1	0.0017	10	10	0.196	0.005	$PM_{1,0}$	5.578	0.0483

Table 2: Summarized of normalization mass (*N*) of $PM_{1.0}$ and $PM_{10.0}$ per one laser shot and 1.0 cm² for substrate sample A1 – A18, B1 – B18 and C1 – C18.

									PM _{10.0}	5.446	0.0471
B1	1	73	1	0.0017	10	10	0.071	0.003	PM _{1.0}	2.453	0.0590
									PM _{10.0} PM _{1.0}	3.878	0.0933
B2	1	77	1	0.0017	10	10	0.071	0.002	$PM_{10.0}$	2.35	0.0565
B3	1	76	1	0.0017	10	10	0.071	0.003	$PM_{1.0}$	2.522	0.0607
20			-	010017	10	10	01071	01002	PM _{10.0} PM _{10.0}	5.364	0.1291
B4	1.5	72	1	0.0017	10	10	0.071	0.004	$PM_{10.0}$	5.512	0.1326
B 5	15	73	1	0.0017	10	10	0.071	0.003	$PM_{1.0}$	1.875	0.0451
20	110	10	-	010017	10	10	01071	01002	PM _{10.0}	4.472	0.1076
B6	1.5	76	1	0.0017	10	10	0.071	0.004	$PM_{10.0}$	7.179	0.1728
B7	2	73	1	0.0017	10	10	0.071	0.002	$PM_{1.0}$	1.814	0.0436
	_		-						PM _{10.0} PM _{10.0}	4.848	0.1167
B8	2	72	1	0.0017	10	10	0.071	0.002	$PM_{10.0}$	3.36	0.0809
B9	2	76	1	0.0017	10	10	0.071	0.003	$PM_{1.0}$	2.204	0.0530
	_		-						PM _{10.0} PM _{10.0}	6.268 4.081	0.1509
B10	1	73	1	0.0017	10	10	0.196	0.005	$PM_{10.0}$	6.839	0.0592
B11	1	76	1	0.0017	10	10	0.196	0.003	$PM_{1.0}$	5.08	0.0440
									PM _{10.0} PM _{1.0}	8.276 5.517	0.0716
B12	1	75	1	0.0017	10	10	0.196	0.002	$PM_{10.0}$	12.48	0.1081
B13	1.5	72	1	0.0017	10	10	0.196	0.005	$PM_{1.0}$	4.671	0.0404
			-						PM _{10.0} PM _{1.0}	7.591 3.774	0.0657
B14	1.5	71	1	0.0017	10	10	0.196	0.006	$PM_{10.0}$	7.686	0.0665
B15	1.5	76	1	0.0017	10	10	0.196	0.003	PM _{1.0}	5.065	0.0438
									PM _{10.0} PM _{1.0}	14.49	0.1255
B16	2	73	1	0.0017	10	10	0.196	0.003	$PM_{10.0}$	4.161	0.0360
B17	2	72	1	0.0017	10	10	0.196	0.004	PM _{1.0}	2.207	0.0191
									$PM_{10.0}$ $PM_{1.0}$	4.349 4.664	0.0376
B18	2	70	1	0.0017	10	10	0.196	0.006	$PM_{10.0}$	7.898	0.0683
C1	1	70	1	0.0017	10	10	0.071	0.007	PM _{1.0}	0.699	0.0167
									$PM_{10.0}$ $PM_{1.0}$	1.592	0.0382
C2	1	71	1	0.0017	10	10	0.071	0.008	$PM_{10.0}$	1.586	0.0380
C3	1	77	1	0.0017	10	10	0.071	0.004	PM _{1.0}	1.086	0.0261
<i></i>		-		0.0015	10	10	0.074	0.000	$PM_{10.0}$ $PM_{1.0}$	0.933	0.0322
C4	1.5	78	I	0.0017	10	10	0.071	0.003	$PM_{10.0}$	1.775	0.0427
C5	1.5	73	1	0.0017	10	10	0.071	0.006	$PM_{1.0}$	1.117	0.0268
06	1.5	70	1	0.0017	10	10	0.071	0.000	$PM_{1.0}$	1.108	0.0265
C6	1.5	/3	1	0.0017	10	10	0.071	0.006	PM _{10.0}	2.536	0.0609
C7	2	76	1	0.0017	10	10	0.071	0.004	PM _{1.0} PM _{1.0}	0.989	0.0237
C	2	70	1	0.0017	10	10	0.071	0.002	$PM_{1.0}$	1.85	0.0445
68	2	/8	1	0.0017	10	10	0.071	0.003	PM _{10.0}	2.635	<mark>0.0634</mark>
C9	2	74	1	0.0017	10	10	0.071	0.006	PM _{1.0} PM	1.512	0.0363
C10	1	70	1	0.0017	10	10	0.106	0.002	$PM_{1.0}$	1.209	0.0105
C10	1	70	1	0.0017	10	10	0.196	0.002	PM _{10.0}	2.086	0.0180
C11	1	71	1	0.0017	10	10	0.196	0.003	PM _{1.0} PM _{10.0}	1.689 2.439	0.0146
C12	1	75	1	0.0017	10	10	0.106	0.005	$PM_{1.0}$	1.418	0.0122
CIZ	1	15	1	0.0017	10	10	0.190	0.005	PM _{10.0}	2.387	0.0206
C13	1.5	78	1	0.0017	10	10	0.196	0.003	PM _{1.0} PM _{10.0}	1.154	0.0100
C14	15	72	1	0.0017	10	10	0 196	0.005	$PM_{1.0}$	2.133	0.0184
017	1.5	12	1	0.0017	10	10	0.170	0.005	PM _{10.0}	2.119	0.0183
C15	1.5	73	1	0.0017	10	10	0.196	0.004	P_{101} PM _{10.0}	2.080	0.0232
C16	2	75	1	0.0017	10	10	0 196	0.004	$PM_{1.0}$	2.641	0.0228
210	-	,5	-	0.0017	10	10	0.170	0.004	PM _{10.0}	3.393	0.0293
C17	2	78	1	0.0017	10	10	0.196	0.002	$PM_{10.0}$	6.555	0.0568
C18	2	80	1	0.0017	10	10	0.196	0.001	PM _{1.0}	5.436	0.0471
									$PM_{10.0}$	5.112	0.0443

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3.1 Factors in producing the PM concentration in laser paint removal

Bar graphs represented the concentrations of $PM_{1.0}$ and $PM_{10.0}$ produced for three types substrate sample A, B and C. The graphs were randomly distributed in term of RR and PW as shown in Figures 5, 6 and 7. This might be due to long PW 100, 200 and 300 ms with small range scale did not give significant impacts in term of irradiation duration. Indeed, lower ranged of RR 1.0, 1.5 and 2.0 Hz also did not give any clear effects as suggested in the literature, where the particles released should be increased as RR increased [18, 19].

However, the normalization mass of PM per one laser shot and 1.0 cm², N for both PM_{1.0} and PM_{10.0} were increased by using higher laser fluence energy ranged from 210 - 300 J/cm² compared to lower laser fluence energy ranged from 60 - 240 J/cm² as shown in the Tables 2. This is because the higher laser fluence energy leads to generate more PM at the painted surface [7, 16]. The results also revealed the application of 3 mm laser BS was produced higher N concentrations compared to 5 mm laser BS. This is due to the higher laser fluence energy range was available at smaller BS as shown in Table 1 will be directly increased the concentration of laser beam [20].

In addition, emission rate of the PM was increased as the painted layer thickness increased, hence increased the hazardous substances released in workplace [7]. It was found that $PM_{1.0}$ and $PM_{10.0}$ concentrations released from sample B was highest due to the thickest of paint material.

Furthermore, surface roughness on the painted material was also influenced particle size distributions, where larger size of PM tends to be generated from the rough surface [16]. However, the surface roughness not considered as a main factors to influence the production of PM concentrations in this study due to the flat uniform surface of non-irradiated sample A, B and C. The results also revealed the air humidity did not give any significant effects to the PM released during laser paint removal. This is because, the humidity in air was dominant in influenced the production of PM for size greater than $20 \ \mu m$ [7].

For this research, the highest *N* of $PM_{1.0}$ and $PM_{10.0}$ were 0.0485 mg/shot/cm² and 0.0766 mg/shot/cm² for Sample A, 0.0890 mg/shot/cm² and 0.1728 mg/shot/cm² for Sample B and 0.0530 mg/shot/cm² and 0.0634 mg/shot/cm² for Sample C, respectively.

3.2 Effects to the paint removal efficiency process

The productions of PM was effected the average coating removal efficiency (ϵ) if the particles released redeposited on the crater surface [16, 21]. However, the plume produced during laser irradiation on painted material is considered as the main factors to effect the process efficiency [18, 19, 22]. This is because some of the laser fluence energy was absorbed by the particle released in air, hence reduced the laser intensity to the next layers of the painted material [21]. Because of that, sample B which produced highest *N* of PM_{1.0} and PM_{10.0} considered to produce lowest ϵ . By the way, lower PM concentrations produced by sample A and C also in lined with their ϵ process, where lower *N* productions of sample A and C give minor effects to the laser fluence energy to reach deep layers of painted material with a few reductions in laser intensity.

IV. Conclusion

The highest *N* of PM_{1.0} and PM_{10.0} measured in a close space were 0.0485 mg/shot/cm² and 0.0766 mg/shot/cm² for Sample A, 0.0890 mg/shot/cm² and 0.1728 mg/shot/cm² for Sample B and 0.0530 mg/shot/cm² and 0.0634 mg/shot/cm² for Sample C, respectively. The lowest C_{av} PM_{1.0} and PM_{10.0} concentrations detected during 10 minute laser irradiation with excluded the C_{noise} were 0.693 mg/m³ and 1.586 mg/m³ as shown in Table 2. The results show both types of PM_{1.0} and PM_{10.0} concentration detected during the laser paint removal process were far exceed from the recommended values suggested by WHO. However, laser paint removal techniques was considered safe compared than chemical paint stripping technique if smooth air ventilation in workplace was properly set-up and inhalation to PM was greatly prevented by using protective mask.

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